Technical Appendix 6-3
Peat Management Plan

EIAR – Volume 3

Muingmore Wind Farm

SLR Project No.: 501.065301.00001

April 2026

Technical Appendix 6.3: Peat Management Plan

Muingmore Wind Farm

RWE Renewables Ireland Limited

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0	12 November 2025	R. Watson	A. Huntridge	A Huntridge
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Basis of Report

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1.0 Introduction

1.1 General

SLR Consulting Ltd (SLR) was commissioned by RWE Renewables Ireland Ltd. (the 'Applicant'), to undertake a Stage 1 Peat Management Plan (PMP) for the proposed Muingmore Wind Farm (the Main Wind Farm Development Site). The location and layout of the Main Wind Farm Development Site are detailed on **Figure 6.3.1** and **Figure 6.3.2** with the red line defining 'the Proposed Development Site boundary'.

The methods adopted for the assessment follow relevant currently available best practice guidance[1] published by the Scottish Environment Protection Agency (SEPA) and wind farm construction good practice guidance.

This PMP has been prepared by a team of Geotechnical Engineers and Geologists, with over 18 years' experience in undertaking peat assessments. The team was led by a Chartered Geologist with 15 years' consultancy experience and specialising in the assessment of soils, geology and water for renewable power projects in Ireland and the UK:

- Paul Gordon (EurGeol PGeo MIMMM) is a Technical Director with SLR and has a BSc in Geology and an MSc in Environmental Management. He has over 20 years' professional experience, primarily in the Irish natural resources industry, including the writing of land, soils and geology chapters for EIARs in Ireland.
- Alan Huntridge (BSc (Hons), MSc) is a Principal in SLR's Land Quality & Remediation team, with 14 years of experience in the sector. Alan was responsible for the Peat Landslide Hazard Risk Assessment, appended to this chapter.
- Ruari Watson (BSc (Hons) Civil Engineering) is an Associate Geotechnical Engineer in SLR's Land Quality & Remediation team, based in Scotland. Ruari has over 12 years' experience within the geotechnical engineering sector. This experience has been gained while working for both specialist contractors and consultants, managing ground investigations and undertaking geotechnical assessments.

The report should be read in conjunction with **Chapter 6** and the following Technical Appendices:

- **Technical Appendix 6-1**: Ground Investigation Factual Report.
- **Technical Appendix 6-2**: Peat Landslide and Hazard Risk Assessment Plan (PLHRA).

1.2 Proposed Project

See **Chapter 2** of this EIAR for a full detailed description of the Proposed Project.

1.3 Objectives

The role of the Stage 1 PMP is to ensure that the management of peat excavated during construction of the Proposed Project will be appropriately managed during the construction process to ensure no negative environmental effects.

The PMP details the overall approach of minimising disruption to peatland, and it ensures that all opportunities to minimise peat disturbance and extraction will be taken during construction of the Proposed Project.

1 Scottish Government, Scottish Natural Heritage, SEPA., (2017) Peatland Survey. Guidance on Developments on Peatland.

The PMP is a working document to be used throughout the key stages of the design, construction, operation, decommissioning and re-instatement phases of the Proposed Project as part of an overall Construction Environmental Management Plan (CEMP).

This PMP will be a key contract document during all stages of the Proposed Project, which will ensure that all mitigation measures, which are considered necessary to manage peat and protect the environment are implemented. This PMP will be updated as required following the grant of permission to incorporate any additional mitigation measures that are considered to be required by the consenting authority.

These stages are outlined below:

Stage 1: Environmental Impact Assessment (EIA)

This report forms the Stage 1 PMP and is submitted as part of the EIA Report. From this initial report, the PMP will be developed further into a Stage 2 Pre-Construction PMP.

Stage 2: Post Consent / Pre-Construction

Following the grant of permission and detailed confirmatory surveys and ground investigations carried out prior to the commencement of construction to confirm the accuracy of the pre-consent assessment of the baseline environment, the PMP will be updated and revised as required to incorporate any additional mitigation measures that are required in accordance with the conditions of any permission.

Stage 3: Construction Stage

Actual peat volumes excavated during construction will be recorded against the overall predicted volumes. A regular review and update of the peat mass balance table will be undertaken by the appointed Contractor and monitored by the Ecological Clerk of Works (ECoW) on-site and made available to regulators as required.

1.4 Guidance

The PMP has been compiled in accordance with the following best practice guidance:

- Scottish Government, Scottish Natural Heritage, SEPA., (2017), Peatland Survey. Guidance on Developments on Peatland[1];
- NatureScot (July 2024), Good Practice During Wind Farm Construction[2];
- Scottish Environment Protection Agency (2010), SEPA Regulatory Position Statement - Developments on Peat[3];
- Scottish Renewables and SEPA (2012), Guidance on the Assessment of Peat Volumes, Reuse of Excavated Peat and the Minimisation of Waste[4];
- Forestry Commission Scotland & Scottish Natural Heritage (2010), Floating Roads on Peat - Report into Good Practice in Design, Construction and Use of Floating Roads on Peat with reference to Wind Farm Developments in Scotland[5].
- Best Practice Guidelines for the Irish Wind Energy; Irish Wind Energy Association (2012).

2 NatureScot (July 2024), Good Practice During Wind Farm Construction. https://www.nature.scot/doc/good-practice-during-wind-farm-construction

3 Scottish Environment Protection Agency. 2010. Regulatory Position Statement – Developments on Peat

4 Scottish Renewables, Scottish Environment Protection Agency. 2012. Guidance on the Assessment of Peat Volumes, Reuse of Excavated Peat and the Minimisation of Waste

5 Scottish Natural Heritage, Forestry Commission (August 2010). Floating Roads on Peat

- Wind Energy Development Guidelines; Department of Housing, Local Government and Heritage (2006).

The guidance listed above has been largely developed by the Scottish Government. In absence of relevant Irish guidance, the Scottish documents are considered to be best practice in Ireland and are therefore appropriate for use within this PMP.

2.0 Baseline Conditions

2.1 Definition of Peat

Peat is defined as an organic soil comprising the partly decomposed plant remains that have accumulated in-situ, rather than being deposited by sedimentation. When peat forming plants die, they do not decay completely as their remains become waterlogged due to regular rainfall. The effect of waterlogging is to exclude air and hence limit the degree of decomposition. Consequently, instead of decaying to carbon dioxide and water, the partially decomposed material is incorporated into the underlying material and the peat 'grows' in-situ.

The Scottish Government Peat Landslide Hazard Best Practice Guide (2017) uses the following Joint Nature Conservation Committee (JNCC) report 455 'Towards an Assessment of the State of UK Peatlands' definition for classification of peat deposits:

- Peaty (or organo-mineral) soil: a soil with a surface organic layer less than 0.5 m deep;
- Peat: a soil with a surface organic layer greater than 0.5 m deep which has an organic matter content of more than 60 %; and
- Deep Peat: a peat soil with a surface organic layer greater than 1.0 m deep.

Peat is characterised by low density, high moisture content, high compressibility and low shear strength, all of which are related to the degree of decomposition and hence residual plant fabric and structure. To some extent, it is this structure that affects the retention or expulsion of water in the system and differentiates one peat from another.

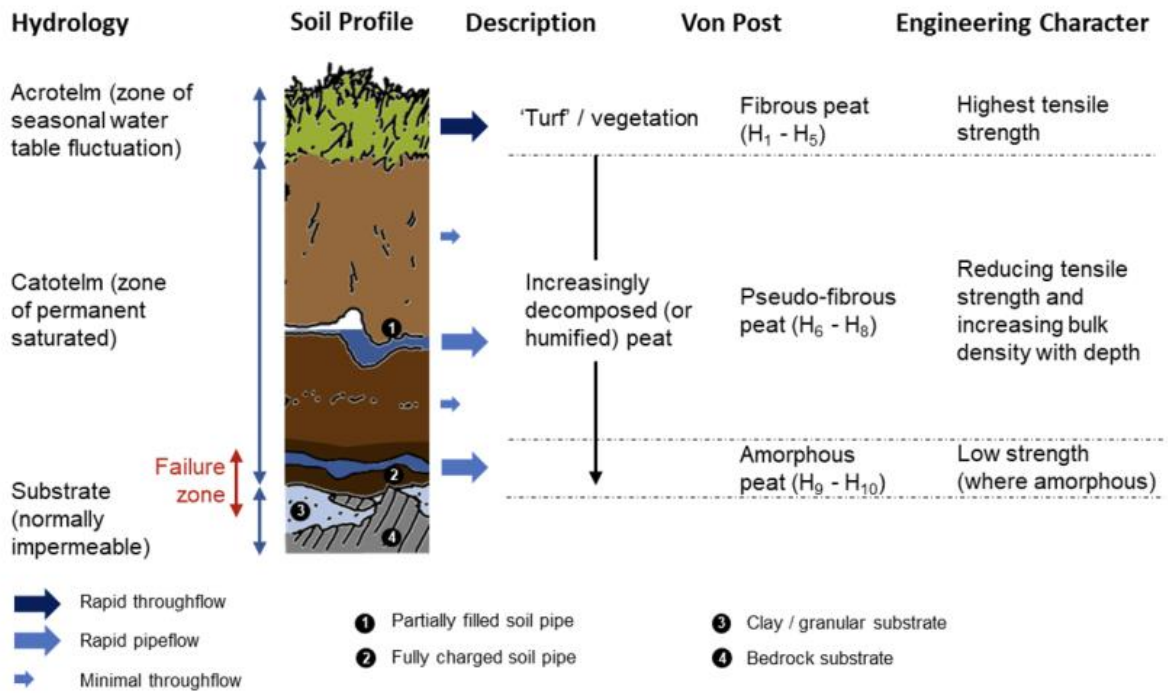
Lindsay[6] defined two main types of peat bog, raised bog and blanket bog, which are prevalent on the West coast of Europe along the Atlantic seaboard. In Ireland, the dominant peatland is blanket bog which occurs on the gentle slopes of upland plateaux, ridges and benches and is predominantly supplied with water and nutrients in the form of precipitation. Blanket peat is usually considered to be hydrologically disconnected from the underlying mineral layer.

There are two principal types of peat in a near natural peatland (see **Plate 1 below**):

- The upper (acrotelm) layer in which the water table fluctuates, which is fibrous and comprises plant roots etc. The acrotelm is relatively dry and has some tensile strength and its thickness typically ranges from 0.1 m to 0.6 m deep.
- The lower (catotelm) layer, which is saturated, sitting permanently below the water table. The catotelm layer is highly decomposed, generally becoming more amorphous/liquid in nature and losing structure with increasing depth. The structure of catotelmic peat tends to disrupt completely on excavation and handling.

6 Lindsay, R.A., (1995), 'Bogs: The ecology, classification and conservation of Ombrotrophic Mires.' Scottish Natural Heritage, Perth.

Plate 1 - Typical Peat Profile[7]



The acrotelm is the fibrous surface to the peat bog[8], typically less than 0.6 m thick, which exists between the growing bog surface and the lowest position of the water table in dry summers.

For geotechnical purposes the degree of decomposition (humification) can be estimated in the field by applying the 'squeezing test' proposed by von Post and Grunland[9] (1926) and as shown in Plate 1. The humification value ranges from H1 (no decomposition) to H10 (highly decomposed). The extended system set out by Hobbs[10] provides a means of correlating the types of peat with their physical, chemical and structural properties.

The relative position of the water table within the peat controls the balance between accumulation and decomposition and therefore its stability, hence artificial adjustment of the water table by drainage requires careful consideration.

2.2 Peat Conditions on Site

The Main Wind Farm Development Site was assessed for peatland in a desktop review of maps and plans (April 2025), historic ground investigation data (April 2025), site walkovers (February 2023) peat surveys (August 2023, September 2024 and February 2025) and ground investigation (September to November 2024).

The Main Wind Farm Development Site is less than 1 km from the Atlantic coastline and is located on low-lying terrain, ranging from approximately 3 m AOD at the southern end to approximately 33 m AOD at the northeastern portion.

The Main Wind Farm Development Site is characterised by commercial forestry and peatland. The Main Wind Farm Development Site features a flat expanse of ground with relatively few changes in elevation. Areas of commercial forestry are noted within the north-west and south

7 Mills, A.J. and Rushton, D. 2023. A risk-based approach to peatland restoration and peat instability. NatureScot Research Report 1259.

8 Ingram, H.A.P., (1978), 'Soil layers in mires: function and terminology'. Journal of Soil Science, 29, 224-227.

9 Von Post, L. and Grunland, E., (1926), 'Sodra Sveriges torvillganger 1' Sverges Geol. Unders. Avh., C335, 1-127.

10 Hobbs, N.B., (1986), 'Mire morphology and the properties and behaviour of some British and foreign peats.' Quarterly Journal of Engineering Geology, London, 19, 7-80.

with peatland covering the remainder of the Main Wind Farm Development Site. Historical peat extraction activities were noted throughout the peatland areas.

3.0 Peat Probing

3.1 Peat Surveys

Peat surveys were carried out in accordance with best practice guidance for developments on peatland[11,12]. Phase 1 peat probing was conducted on a 100 m grid (August 2023) to allow for initial assessment of the Main Wind Farm Development Site which was used in preliminary site layout designs. Phase 2 probing saw detailed probing undertaken across the Main Wind Farm Development Site layout (September 2024), focussing on access tracks, turbines, hardstandings and other site infrastructure. Phase 2 probing was undertaken on linear infrastructure (tracks and cable routes) at 50 m spacings with offset probing locations either side (approximately 10 m to 25 m). Infrastructure (turbines, hardstandings, compounds, etc.) was probed at 10 m grid spacings. Where upgraded infrastructure is proposed (access tracks, cable routes in track alignments), probing was undertaken adjacent to existing infrastructure (existing tracks) where possible. Additional phase 2 probing was undertaken in February 2025 to pick up gaps in the probing grids due to design changes.

The thickness of the peat was assessed using a graduated peat probe, approximately 6 mm in diameter and capable of probing depths of up to 10 m. This was pushed vertically into the peat to refusal and the depth recorded, together with a unique location number and the co-ordinates from a handheld Global Positioning System instrument (GPS). The accuracy of the GPS was quoted as ±2 m, which was considered sufficiently accurate for this survey. All data was uploaded into a GIS database for incorporation into various drawings and analysis assessments.

3.2 Results

As detailed in Section 2.1, peat is generally defined as a soil with a surface organic layer in excess of 0.5 m[11]. Where the probing recorded less than 0.5 m thick, it is considered to be a peaty soil (or organo-mineral soil). Soils with a peaty organic horizon over mineral soil are often referred to as ‘peaty soils’. These organo-mineral soils are extensive across the UK and Ireland uplands, but do not meet recognised definitions of peat as they are either shallower than true peat or have a lower carbon density.

The peat depth is shown on **Figure 6.3.3.** The interpolation was undertaken using the Spline with Barriers tool in ArcGIS Pro.

A total of 3,379 peat probes were undertaken across all survey phases (August 2023, September 2024 and February 2025). Table A summarises the peat probing results below. The average thickness of peat recorded across the Main Wind Farm Development Site was 2.5 m. The maximum depth of recorded peat was 6.4 mbgl, near T7.

Table A: Peat Probing Results

Peat Thickness (m)	**No. of Probes**	**Percentage (of total probes undertaken on-site)**
0 (no peat)	144	4.3
0.01 – 0.49 (peaty soil)	49	1.5
0.50 – 0.99	170	5.0
1.00 – 1.49	215	6.4

11 Scottish Renewables & SEPA (2012) ‘Developments on Peatland Guidance on the Assessment of Peat Volumes, Reuse of Excavated Peat and the Minimisation of Waste’.

12 Scottish Natural Heritage (SNH), SEPA, Scottish Government & James Hutton Institute. (2014)’ Peat Survey Guidance; Developments on Peatland: Site Surveys’.

Peat Thickness (m)	**No. of Probes**	**Percentage (of total probes undertaken on-site)**
1.50 – 1.99	319	9.4
2.00 – 2.49	615	18.2
2.50 – 2.99	636	18.8
3.00 – 3.49	750	22.2
3.50 – 3.99	281	8.3
> 4.0	200	5.9

4.0 Ground Investigation

SLR instructed Irish Drilling Ltd. (IDL) to carry out a ground investigation (GI) at the Main Wind Farm Development Site. The GI was undertaken to provide detailed factual geotechnical information of the underlying ground conditions at the Main Wind Farm Development Site. The fieldwork commenced in September 2024 and was completed in November 2024.

4.1 Fieldwork

The ground investigation was carried out in accordance with the current best practice IS EN 1997-2 and BS5930:2015+A1:2020 Code of Practice for Ground Investigations with precedence given to IS EN 1997-2 where applicable. The results of the GI are presented within **Technical Appendix 6-1**.

A summary of the fieldwork is detailed in Table B.

Table B: Summary of Fieldwork

Exploratory Hole Type	Number of Locations	Exploratory Hole Reference IDs	Depth Range (mbgl)
Rotary Cored Boreholes	16	BH-01 to BH-13, BH-MM1, BH-MM2 & BH-SS	8.60 – 20.30
Machine Excavated Trial Pits	32	TP-01 to TP-26, TP-28 to TP-32 & TP-CC	2.20 – 4.50

4.2 Laboratory Testing

A series of laboratory tests were undertaken by IDL, on selected samples recovered from the exploratory locations. The tests and total number completed are summarised in Table C.

Table C: Summary of Laboratory Testing

Laboratory Test	Number of Tests
Moisture content	45
Atterberg Limits	8
Particle size distribution	9
Chemical (Sulphate, Total)	7
Chemical (Total Sulphur)	56
UCS	12
Point Load	14

4.3 Ground Conditions

It should be noted there were a number of turbine locations that were inaccessible due to extensive forestry across the Main Wind Farm Development Site. Some of the exploratory hole locations were positioned out with the footprint of the proposed turbine locations. The following is presented as an indication of the possible ground conditions expected to be encountered. Engineering judgement has been used to assess and summarise the available ground investigation data and provide a robust assessment based on the information available.

Made ground was noted across the site where trial pits were excavated through the existing access track make-up. Made ground thickness ranged from 0.3 to 1 mbgl and typically comprised existing granular track make-up of reworked material from previous construction of tracks.

The intrusive phase of investigation has confirmed the presence of variable peat thicknesses overlying till deposits, with a maximum depth of 5.6 mbgl recorded at BH-13.

Till deposits were encountered underlying the peat consisting of generally granular material. Cohesive material described as silt was also encountered in thin layers throughout the superficial material. The till was encountered underlying the peat between 1 to 5.6 mbgl.

Bedrock was proven across the Main Wind Farm Development Site and consisted of the Annagh Division and generally described as medium strong to very strong Orthogneiss. The bedrock was encountered underlying the superficial material between 3.55 to 13.9 mbgl. Bedrock was proven to a maximum depth of 20.3 mbgl in BH-07.

Groundwater was encountered at the Main Wind Farm Development Site with trial excavations between 1.1 to 3.7 mbgl.

5.0 Peat Management and Mitigation

The Proposed Project design took account of a number of environmental and technical constraints. Where peat is to be excavated, re-used or reinstated, the following sections detail good practice which applies to protect carbon rich soils and mitigate impacts to peat.

For the construction phase of the Proposed Project, the following activities are considered to have an impact on peatland:

- Construction of:
  - New permanent access tracks;
  - Site access entrances;
  - Turbine foundations;
  - Hardstanding foundations;
  - Substation foundation;
  - BESS foundation;
  - Met mast; and
  - Temporary construction compounds.

Given the current infrastructure design proposals and layout, no surplus peat is expected to be generated by the Proposed Project. The majority of the Proposed Project will utilise floating and piled foundation solutions to minimise significant peat excavation. The estimated peat excavation volumes will be reused for restoration purposes during the construction, operational, and decommissioning phases of the project. Peat management and mitigation of the above construction activities are covered individually in the following sections.

5.1 Turbine Foundations

The bases of the turbine foundations will be excavated to a competent-bearing stratum or founded on piles. Ground investigations to date have provided an indication of the possible ground conditions expected to be encountered at the proposed turbine locations. Peat greater than 1 m was encountered at the majority (12 of 13) of turbine locations. Hence, based on the available ground investigation data it is assumed that most of the turbine foundations will utilise a piled solution, with the potential for a small number to be gravity foundations based on depths to competent strata.

The process of piling specific infrastructure will be carried out in line with the appointed contractor's method statement. The final pile type and installation method shall be determined by detailed ground investigation results, accounting for peat characteristics, underlying strata and environmental constraints. Piling methods may include:

- Bored Piles with Temporary Casing - Suitable in saturated or unstable peat to prevent ingress or instability.
- Continuous Flight Auger - Typically used where bore stability can be maintained and groundwater inflow is manageable.

5.2 Hardstanding Foundations

Each turbine will have a turbine hardstanding area constructed to provide solid area for the main installation crane that will be used to backfill the turbine and for the assembly of the turbine.

Areas of the crane pad that are not required to directly support loads imposed by the crane, will be designed as floating pads, utilizing a combination of geogrid and crushed stone to create a stable platform.

For crane erection at hardstandings, a piled crane pad will be constructed to support the main crane, with a designated area on the crane hardstanding identified for this purpose. This method will involve installing piles that extend to rock and construction of a pad supported on these piles. To minimise peat excavation and disturbance, the piled crane pad will be limited in size to include the crane with its outriggers. This design will be undertaken by a suitably qualified engineer and crane specialist to ensure it meets the requirements of the Health and Safety Authority (HSA) regulations.

For the remainder of the crane pad around the piled outriggers, a design incorporating a geogrid, or similar geosynthetic material, and engineered fill will be completed. This is subject to each hardstand location and its ground conditions.

Crane pads will remain in place for the operational life of the project, with stored topsoil and peat being used to restore the edges, blade laydowns and jib assembly areas.

5.3 New Tracks

Access tracks will be required as part of the Proposed Project to provide access to the turbine locations. Approximately 6.8 km of new access track will be constructed and 1.95 km of existing access track upgraded.

Ground investigations, including trial pitting and peat probing, have confirmed that deep peat (greater than 1 m) is encountered across the Main Wind Farm Development Site. Therefore, it is proposed that access track construction will be floated and therefore, excavations are not required.

5.3.1 Floating Track Construction

The design and use of floating track construction is documented in several guidance documents[2,5] which will be followed during access track design in peatlands. Floating roads are constructed directly on top of peat and soft soils. Where peat depths exceed 1 m, floating road construction will be adopted. Access tracks will typically be built to an average height of 0.5 m above the existing ground level.

The design of floating track sections will be carried out either by a geogrid manufacturer, a consultant working in collaboration with a geogrid supplier, or by an experienced contractor with expertise in constructing roads over peat. Specific mitigation measures for the design and use of floating tracks are highlighted below:

- An increased width of reinforced earth construction will be used where applicable. The construction design will allow for an increased width of geo-grid layers beneath the track which will extend outwards from beneath the running surface. This will generally have the effect of spreading loads over a wider area and reduce the risk of shear failure.
- Load movements along critical sections of access track will be safely managed during the planning process. All tracks will be centrally loaded by large cranes and other heavy plant machinery. This will reduce the risk of shear failure and differential settlement of the access tracks.
- Peat deposits have very low shear strength. Where provision for floating track design is made, aggregate material will be to an agreed specification such as MCHW Series 600 Earthworks well graded granular selected fill to structures and reinforced earth (e.g. 6F2, 6N or 6J).

- Road performance will be enhanced by the use of suitable geo-textile at formation level and incorporating at least one geo-grid layer. All fills will be compacted in accordance with best engineering practice. Non vibratory compaction methods will be used for fill over peat.
- Basal geo-grids will be laid directly onto the existing ground surface, i.e. the surface layer of peat vegetation need not be stripped. Major protrusions such as rocks, large tree stumps, bushes, etc. will need to be removed, and hollows infilled.
- Side slopes and adverse gradients (>5°) are likely to be unsuitable for floating type access tracks and therefore, excavated track is required.

5.4 Temporary Construction Compound

Prior to the construction of the wind turbine infrastructure, temporary construction compounds will be required to provide office space, welfare facilities, concrete wash out areas, hardstandings for storing materials and hazardous materials. The compounds will be floated and will be subject to maintenance and upkeep. Due to them being temporary, there is no need for a piled solution. Specific mitigation measures for the design of the construction compounds are highlighted below:

- An increased width of reinforced earth construction will be used where applicable. The construction design will allow for an increased width of geo-grid layers beneath the compounds will extend outwards from beneath the footprint. This will generally have the effect of spreading loads over a wider area and reduce the risk of shear failure.
- Peat deposits have very low shear strength. The aggregate material used within the design will be to an agreed specification such as MCHW Series 600 Earthworks well graded granular selected fill to structures and reinforced earth (e.g. 6F2, 6N or 6J).
- Hardstanding performance will be enhanced by the use of suitable geo-textile at formation level and incorporating at least one geo-grid layer. All fills will be compacted in accordance with best engineering practice. Non vibratory compaction methods will be used for fill over peat.
- Basal geo-grids will be laid directly onto the existing ground surface, i.e. the surface layer of peat vegetation need not be stripped. Major protrusions such as rocks, large tree stumps, bushes, etc. will need to be removed, and hollows infilled.

5.5 BESS and Substation

The Proposed Project includes the construction of a BESS facility and substation building. Both developments will require a concrete platform to be constructed as a foundation base. The construction of the substation and BESS foundations will require the full excavation of peat. Peat will be re-used around the perimeter of the BESS and substation and within peatland restoration as detailed within Section 5.6.3. Specific mitigation measures for the design of the BESS and Substation will be in accordance with those detailed in Section 5.6.

5.6 General Good Practice

5.6.1 Peat Transport and Handling

The following good practice and mitigation will be implemented to peat transport:

- movement of turves will be kept to a minimum once excavated, and therefore it is required to transport peat planned for translocation and reinstatement to its destination at the time of excavation; and

- peat materials will be separated from non-peat materials prior to transportation around the Main Wind Farm Development Site to minimise cross-contamination.

Following refinement of the peat model, a detailed storage and handling plan will be prepared forming part of the updated CEMP, including details of:

- the storage mitigation measures detailed in Section 5;
- best estimate excavation volume at each infrastructure location (including peat volumes split into area/volume of 'acrotelm' or 'turf', and volume of catotelm) which would be achieved by undertaking additional probing in line with current guidance;
- volume to be stored locally and volume to be transferred directly on excavation to restoration areas elsewhere (e.g. peat storage areas) in order to minimise handling;
- location and size of storage area relative to turbine foundations and infrastructure locations and natural peat morphology / drainage features; and
- irrigation requirements and methods to minimise desiccation of excavated peat during short term storage.

These parameters are best determined post-consent, informed by detailed ground investigation.

5.6.2 Storage

The following good practice and mitigation measures will be implemented when storing peaty soils/peat:

- stripped materials will be carefully separated to keep peat and other type of soils apart;
- to minimise handling and haulage distances, excavated material will be stored local to the site of excavation and/or end point of restoration;
- peat turves will be stored in wet conditions and/or irrigated in order to prevent desiccation (once dried, peat will not rewet);
- stockpiling of peat will be in large volumes to minimise exposure to wind and sun (and desiccation), but with due consideration for slope stability, but will not exceed 1 m in height to maintain stability of stockpile;
- stockpiles will be isolated from watercourses or drains with appropriate bunding to minimise pollution risks;
- to be stored a minimum of 10 m from any watercourse;
- stores of non-turf (catotelm) peat will be bladed off to reduce the surface area and desiccation of the stored peat; and
- peat storage areas will be monitored during periods of very wet weather, or during snowmelt, to identify early signs of peat instability.

Any peaty soils/peat to be removed during construction will be stored in temporary storage area near to the construction works/area of re-use. Where peat cannot be transferred immediately to an appropriate restoration area, short term storage will be required. In this case, the following good practice and mitigation measures will be implemented:

- peat will be stored around the excavation perimeter at sufficient distance from the cut face to prevent overburden induced failure;
- local gullies, diffuse drainage lines (or very wet ground) and locally steep slopes will be avoided for peat storage;

- drying of stored peat will be avoided by irrigation or by seeding (although this is unlikely to be significant for peat materials stored for less than 2 months);
- peat generated from permanent excavations will be transported directly to its allocated restoration location, to minimise the volume being stockpiled with the possibility of drying out;
- stores of catotelm peat will be bladed off to reduce their surface area and minimise desiccation;
- where transport cannot be undertaken immediately, stored peat will be irrigated to limit drying and stored on a geotextile mat to promote stability; and
- monitoring of large areas of peat storage during wet weather or snowmelt will be undertaken to identify any early signs of peat instability.

5.6.3 Restoration

Peatland restoration will be undertaken across various areas of the site to re-use peat excavated as part of the Proposed Project. Up to 101,301 m^3 of excavated peat from construction may be utilised within peatland restoration via ditch blocking. Full details of the peatland restoration proposal are detailed within **Chapter 5** and **Technical Appendix 5-5**. The methodologies detailed in any future restoration scheme will be followed as well as the following best practice measures which will be implemented:

- carefully evaluate potential restoration sites, such as peat storage areas for their suitability, and agree that these sites are appropriate with the ECoW, landowners and relevant consultees;
- undertake restoration and revegetation or reseeding work as soon as practically possible;
- where required, consider exclusion of livestock from areas of the Proposed Project undergoing restoration, to minimise impacts on revegetation; and
- as far as reasonably practicable, restoration will be carried out concurrently with construction rather than at its conclusion.

5.6.4 Monitoring and Inspection

There will be frequent, routine and regular inspections of peat in all stockpiles and temporary storage areas as part of the PMP audit process. Inspections will assess in situ peat physical conditions, integrity of containment and temporary drainage conditions, and they will seek to confirm that stockpile design and management was adequate to prevent erosion and peat slide. These inspections will take place weekly during stockpile creation and storage.

Should any problems be observed during regular visual inspections of peat stockpiles, this will invoke implementation of an appropriate corrective action which will be recorded and monitored for effectiveness. The following corrective actions will be implemented as required:

- modification of temporary drainage, to ensure peat stockpiles remain saturated;
- additional or modified bunding, to ensure stability within storage areas;
- incorporating of sediment fencing; to prevent sediment run-off effecting the environment;
- light re-grading to correct any areas of surface erosion, to stop desiccation of peat materials.

Regular, frequent inspections of peat conditions during construction and restoration phases of work will be carried out by the Engineer and ECoW as follows:

- peat surface, peat profile and peat consistency conditions will be carried out as part of ground investigations prior to the start of construction. This information will provide detailed information on the baseline conditions for each part of the infrastructure footprint;
- restored peat conditions will be inspected immediately after restoration to ensure that the methods detailed in the PMP had been correctly implemented and to inform any corrective actions should they be required;
- further monitoring to be undertaken where required to ensure restoration works have been correctly implemented; and
- the physical condition of peat will be retained as carefully as possible both at the peat storage and the peat restoration stages. This is particularly important for vegetation establishment.

6.0 Excavated Materials Assessment

Peat excavation volumes associated with the construction of the Proposed Project have been calculated using the results from the peat depth surveys. The interpolation of peat depth was undertaken using Arc GIS and the Spline interpolation method.

Table D provides an estimate of peat volumes to be excavated during the construction of the Proposed Project. The peat excavation volumes are detailed for each infrastructure element in **Annex A**.

Table D: Peat Balance Assessment

Infrastructure	Volume of Peat Excavated (m^3)	Volume of Peat Re-use (m^3)	Proposed Re-use Comments
New Access Track	0	8,758	Assumes all tracks on site where peat >1.0 m and <5 deg slope will be floated construction. Peat to be re-used around verges of new tracks.
Turbines (all turbines)	12,644	455	To be excavated and peat more than 1 m deep spread around the circumference of turbine.
Hardstandings (to be floated)	0	0	To be floated.
Blade Laydown Areas (to be floated)	0	0	To be floated.
Crane Pad (to be piled)	0	0	To utilise piled foundation solution.
Hardstandings (T10 & T11 only)	8,603	2,208	To be re-used in local area and peatland restoration.
Blade Laydown Areas (T10 & T11 only)	11,267	11,267	To be fully reinstated.
Crane Pad (T10 & T11 only)	1,358	442	To be re-used in local area and peatland restoration.
Battery Energy Storage System (BESS)	28,957	380	To be re-used within local area. To be used within peatland restoration as detailed within **Chapter 5** and **Technical Appendix 5-5**.
Substation	29,983	370	To be re-used within local area. To be used within peatland restoration as detailed within **Chapter 5** and **Technical Appendix 5-5**.
Temporary Construction Compound (TCC) 1	0	0	To be floated.
Temporary Construction Compound (TCC) 2	0	0	To be floated.
Met Mast	0	0	To be floated.
Attenuation Ponds	14,269	0	

Infrastructure	Volume of Peat Excavated (m^3)	Volume of Peat Re-use (m^3)	Proposed Re-use Comments
Peatland Restoration	0	101,301	As detailed within **Chapter 5** and Technical **Appendix 5-5**.
Total	107,080	125,180	The potential volume of peat reuse is greater than that excavated to demonstrate that there will be no surplus.

7.0 Conclusion

This Stage 1 PMP presents a pre-construction assessment of the expected peat extraction and reuse volumes associated with the works phase of the construction of the Proposed Project. The PMP described the mitigation and monitoring measures that will be implemented to ensure that peat is appropriately managed during construction activities.

The Main Wind Farm Development Site is generally characterised by commercial forestry and drained lowland blanket bog within a previously cutover bog area. The Main Wind Farm Development Site features a flat expanse of ground with relatively few changes in elevation. Areas of commercial forestry are noted within the north-west and south of the Main Wind Farm Development Site with peatland covering the remainder of the Main Wind Farm Development Site. Historical peat extraction activities were noted throughout the peatland areas.

A total of 3,379 peat probes were undertaken across all survey phases. The average thickness of peat recorded across the Main Wind Farm Development Site was 2.5 m. The maximum depth of recorded peat was 6.4 mbgl, near T7.

The total volume of excavated peat associated with the wind farm infrastructure footprint is estimated at approximately 107,080 m³. Based on peat depth, characteristics, and distribution assessments carried out across the development area, all excavated peat is planned for on-site reuse and peatland restoration.

Given the current infrastructure design proposals and layout and, surplus peat is expected to be generated by the Proposed Project. It is proposed that the majority of the Proposed Project will either utilise a floating or piled foundation solution which removes the requirement for significant peat excavations. The estimated peat excavation volumes will be reused for restoration purposes during the construction, operational, and decommissioning phases of the project.

To minimise excavation volumes, floating roads and other peat-sensitive construction methods will be employed throughout the Main Wind Farm Development Site. An Ecological Clerk of Works (ECoW) will maintain a detailed log of the actual volumes of peat excavated and reused. This record will be updated throughout all phases of the project and made available to relevant regulatory authorities upon request.

Figures

Technical Appendix 6.3: Peat Management Plan

Muingmore Wind Farm

RWE Renewables Ireland Limited

SLR Project No.: 501.065301.00001

460000 465000 470000 475000 480000 485000 490000

835000 830000 825000 820000 815000

402.064443.00001.0126.0 Site Location

L1201 L1201 L1202 L1203 R314 R314 R314 R314 R314 L1204 L1204 L1204 R313 R313 R313 R313 R313 R313 L1205 L5285 L1205 N59 N59 N59 N59 N59 N56 N60

Béal an Mhuirthead

An Geata Mór

Bun na hAbhna

Loch na Ceathrún Móire

Blacksod Bay - Cuan an Fhóid Duibh

Bangor Erris

An Eachléim

An Fál Mór

Ballycroy

Tóin an tSeanbhaile

Galway

N

LEGEND

Proposed Development Site Boundary

Proposed Turbine Location

0 2.5 5

Kilometres

RWE

SLR

MUINGMORE WIND FARM

PEAT MANAGEMENT PLAN

SITE LOCATION

FIGURE 6-3-1

Scale 1:100,000 @ A3

Date MARCH 2026

474000
476000
478000
824000
822000
402.064443.00001.0127.0 Site Layout

N

T1
T2
T3
T4
T5
T6
T7
T8
T9
T10
T11
T12
T13
TCC1
TCC2
1
2
3

L1205
L1206
Saint Colmcille's Church

0
0.5
1
Kilometres

LEGEND

- Proposed Development Site Boundary
- Proposed Turbine Location
- Proposed Site Access Location
- Proposed Met Mast Location
- Proposed New Access Track
- Proposed Upgraded Access Track
- Proposed Grid Connection Route (Subject to Seperate Planning Application)
- Proposed Crane Pad
- Proposed Substation (Indicative Size and Location)
- Battery Energy Storage System (BESS) Compound (Indicative Size and Location)
- Proposed Temporary Construction Compound (TCC)
- Proposed Drainage Feature
- Proposed Attenuation Basin

RWE

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MUINGMORE WIND FARM

PEAT MANAGEMENT PLAN

SITE LAYOUT

FIGURE 6-3-2

Scale 1:18,000 @ A3

Date MARCH 2026

474000 475000 476000 477000 478000 479000

824000 823000 822000

L1205 L1206

FIGURE 6-3-3b FIGURE 6-3-3c FIGURE 6-3-3d FIGURE 6-3-3e FIGURE 6-3-3f FIGURE 6-3-3g FIGURE 6-3-3h FIGURE 6-3-3i FIGURE 6-3-3j

T1 T2 T3 T4 T5 T6 T7 T8 T9 T10 T11 T12 T13

TCC1 TCC2

1 2 3

Saint Colmcille's Church

N

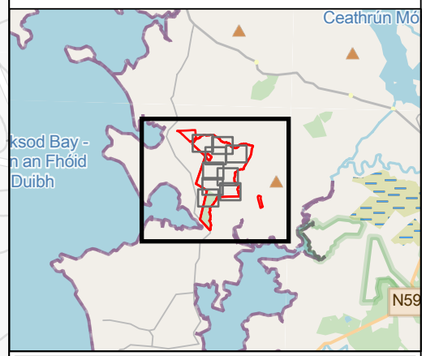
0 0.5 1 Kilometres

LEGEND

- Proposed Development Site Boundary
- Proposed Turbine Location
- Proposed Site Access Location
- Proposed Met Mast Location
- Proposed New Access Track
- Proposed Upgraded Access Track
- Proposed Grid Connection Route (Subject to Seperate Planning Application)
- Proposed Crane Pad
- Proposed Substation (Indicative Size and Location)
- Battery Energy Storage System (BESS) Compound (Indicative Size and Location)
- Proposed Temporary Construction Compound (TCC)
- Proposed Drainage Feature
- Proposed Attenuation Basin
- Peat Probe Location

Peat Depth (m)

- 0
- 0 - 0.5
- 0.5 - 1
- 1 - 1.5
- 1.5 - 2
- 2 - 2.5
- 2.5 - 3
- > 3



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PEAT MANAGEMENT PLAN

PEAT DEPTH DETAILED

FIGURE 6-3-3a

Scale 1:18,000 @ A3

Date MARCH 2026

402.064443.00001.0128.0 Peat Depth Detailed

475600 475800 476000 476200 476400

824000 823800

T1 T2 1

20

N

LEGEND

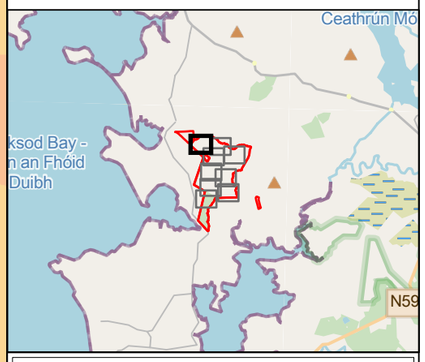
Proposed Development Site Boundary
Proposed Turbine Location
Proposed Site Access Location
Proposed New Access Track
Proposed Crane Pad
Proposed Drainage Feature
Proposed Attenuation Basin

Peat Probe Depth (m)

0
0 - 0.5
0.5 - 1
1 - 1.5
1.5 - 2
2 - 2.5
2.5 - 3
>3

Peat Depth (m)

0
0 - 0.5
0.5 - 1
1 - 1.5
1.5 - 2
2 - 2.5
2.5 - 3
> 3



0 100 200
Meters

RWE

SLR

MUINGMORE WIND FARM

PEAT MANAGEMENT PLAN

PEAT DEPTH DETAILED

FIGURE 6-3-3b

Scale 1:2,500 @ A3

Date MARCH 2026

402.064443.00001.0128.0 Peat Depth Detailed

476400 476600 476800 477000 477200

824000

823800

823600

T3

T5

20

20

20

N

0 100 200

Meters

LEGEND

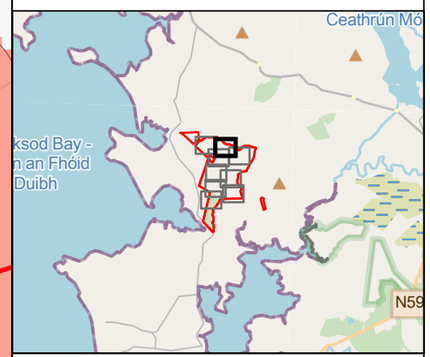
- Proposed Development Site Boundary
- Proposed Turbine Location
- Proposed New Access Track
- Proposed Upgraded Access Track
- Proposed Crane Pad
- Proposed Substation (Indicative Size and Location)
- Battery Energy Storage System (BESS) Compound (Indicative Size and Location)
- Proposed Drainage Feature
- Proposed Attenuation Basin

Peat Probe Depth (m)

- 0
- 1 - 1.5
- 1.5 - 2
- 2 - 2.5
- 2.5 - 3
- >3

Peat Depth (m)

- 0
- 0 - 0.5
- 0.5 - 1
- 1 - 1.5
- 1.5 - 2
- 2 - 2.5
- 2.5 - 3
- > 3



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SLR

MUINGMORE WIND FARM

PEAT MANAGEMENT PLAN

PEAT DEPTH DETAILED

FIGURE 6-3-3c

Scale 1:2,500 @ A3

Date MARCH 2026

402.064443.00001.0128.0 Peat Depth Detailed

476200 476400 476600 476800

823600 823400 823200

N

LEGEND

Proposed Development Site Boundary
Proposed New Access Track
Proposed Upgraded Access Track
Proposed Grid Connection Route (Subject to Seperate Planning Application)
Proposed Crane Pad
Proposed Substation (Indicative Size and Location)
Battery Energy Storage System (BESS) Compound (Indicative Size and Location)
Proposed Temporary Construction Compound (TCC)
Proposed Drainage Feature
Proposed Attenuation Basin

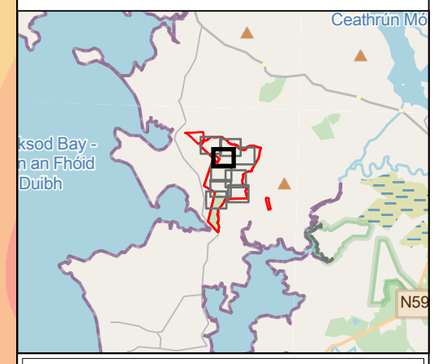
Peat Probe Depth (m)
0
0 - 0.5
1 - 1.5
1.5 - 2
2 - 2.5
2.5 - 3
>3

Peat Depth (m)
0
0 - 0.5
0.5 - 1
1 - 1.5
1.5 - 2
2 - 2.5
2.5 - 3
> 3

TCC1

20 30 20

0 100 200
Meters



RWE

SLR

MUINGMORE WIND FARM

PEAT MANAGEMENT PLAN

PEAT DEPTH DETAILED

FIGURE 6-3-3d

Scale 1:2,500 @ A3

Date MARCH 2026

402.064443.00001.0128.0 Peat Depth Detailled

477000
477200
477400
477600
823600
823400
402.064443.00001.0128.0 Peat Depth Detailled
T5
T7
T4
T6
20
N
0
100
200
Meters

LEGEND

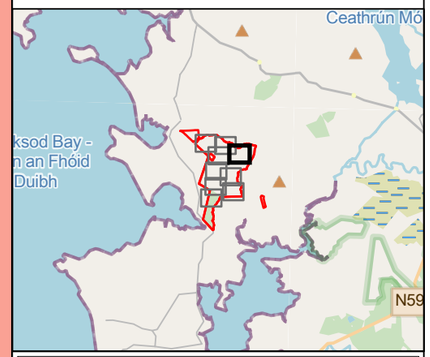
- Proposed Development Site Boundary
- Proposed Turbine Location
- Proposed New Access Track
- Proposed Upgraded Access Track
- Proposed Crane Pad
- Proposed Drainage Feature
- Proposed Attenuation Basin

Peat Probe Depth (m)

- 0
- 0 - 0.5
- 0.5 - 1
- 1 - 1.5
- 1.5 - 2
- 2 - 2.5
- 2.5 - 3
- >3

Peat Depth (m)

- 0
- 0 - 0.5
- 0.5 - 1
- 1 - 1.5
- 1.5 - 2
- 2 - 2.5
- 2.5 - 3
- > 3



RWE

SLR

MUINGMORE WIND FARM

PEAT MANAGEMENT PLAN

PEAT DEPTH DETAILED

FIGURE 6-3-3e

Scale 1:2,500 @ A3

Date MARCH 2026

476000 476200 476400 476600 476800

823000 822800 822600

N

T8 TCC2 2 3

0 100 200
Meters

LEGEND

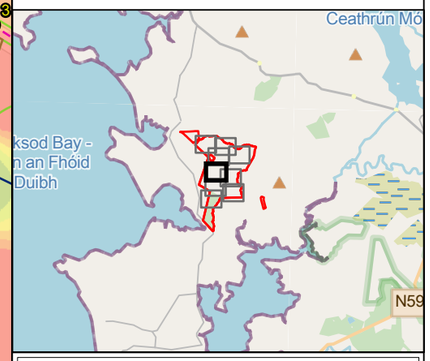
- Proposed Development Site Boundary
- Proposed Turbine Location
- Proposed Site Access Location
- Proposed Met Mast Location
- Proposed New Access Track
- Proposed Upgraded Access Track
- Proposed Grid Connection Route (Subject to Seperate Planning Application)
- Proposed Crane Pad
- Proposed Temporary Construction Compound (TCC)
- Proposed Drainage Feature
- Proposed Attenuation Basin

Peat Probe Depth (m)

0
0 - 0.5
0.5 - 1
1 - 1.5
1.5 - 2
2 - 2.5
2.5 - 3
>3

Peat Depth (m)

0
0 - 0.5
0.5 - 1
1 - 1.5
1.5 - 2
2 - 2.5
2.5 - 3
> 3



RWE

SLR

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PEAT MANAGEMENT PLAN

PEAT DEPTH DETAILED

FIGURE 6-3-3f

Scale 1:2,500 @ A3

Date MARCH 2026

402.064443.00001.0128.0 Peat Depth Detailed

476000 476200 476400 476600 476800

822400 822200 822000

N

T9

T11

20

0 100 200

Meters

LEGEND

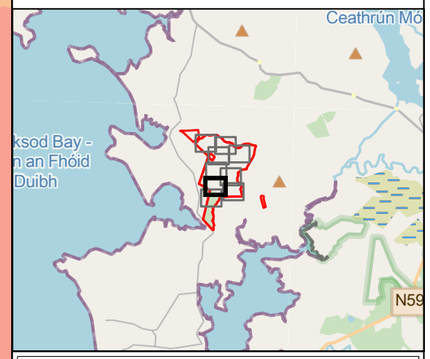
- Proposed Development Site Boundary
- Proposed Turbine Location
- Proposed New Access Track
- Proposed Upgraded Access Track
- Proposed Crane Pad
- Proposed Drainage Feature
- Proposed Attenuation Basin

Peat Probe Depth (m)

- 0
- 0 - 0.5
- 0.5 - 1
- 1 - 1.5
- 1.5 - 2
- 2 - 2.5
- 2.5 - 3
- >3

Peat Depth (m)

- 0
- 0 - 0.5
- 0.5 - 1
- 1 - 1.5
- 1.5 - 2
- 2 - 2.5
- 2.5 - 3
- > 3



RWE

SLR

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PEAT MANAGEMENT PLAN

PEAT DEPTH DETAILED

FIGURE 6-3-3g

Scale 1:2,500 @ A3

Date MARCH 2026

402.064443.00001.0128.0 Peat Depth Detailled

475800 476000 476200 476400 476600

821800

821600

402.064443.00001.0128.0 Peat Depth Detailled

N

T11

T10

20

10

0 100 200

Meters

LEGEND

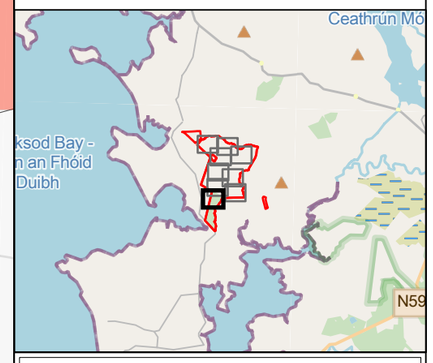
- Proposed Development Site Boundary
- Proposed Turbine Location
- Proposed New Access Track
- Proposed Upgraded Access Track
- Proposed Crane Pad
- Proposed Drainage Feature
- Proposed Attenuation Basin

Peat Probe Depth (m)

- 0
- 0 - 0.5
- 0.5 - 1
- 1 - 1.5
- 1.5 - 2
- 2 - 2.5
- 2.5 - 3
- >3

Peat Depth (m)

- 0
- 0 - 0.5
- 0.5 - 1
- 1 - 1.5
- 1.5 - 2
- 2 - 2.5
- 2.5 - 3
- > 3



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MUINGMORE WIND FARM

PEAT MANAGEMENT PLAN

PEAT DEPTH DETAILED

FIGURE 6-3-3h

Scale 1:2,500 @ A3

Date MARCH 2026

476600 476800 477000 477200 477400

822800 822600 822400

TCC2

T3

T13

N

LEGEND

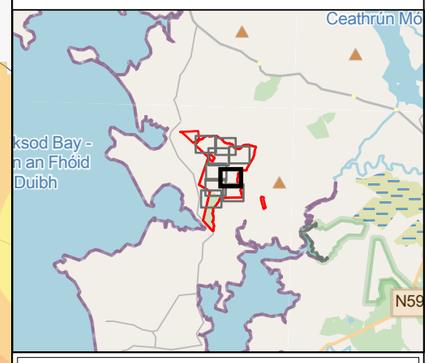
- Proposed Development Site Boundary
- Proposed Turbine Location
- Proposed Site Access Location
- Proposed New Access Track
- Proposed Upgraded Access Track
- Proposed Grid Connection Route (Subject to Seperate Planning Application)
- Proposed Crane Pad
- Proposed Temporary Construction Compound (TCC)
- Proposed Drainage Feature
- Proposed Attenuation Basin

Peat Probe Depth (m)

- 0
- 0 - 0.5
- 0.5 - 1
- 1 - 1.5
- 1.5 - 2
- 2 - 2.5
- 2.5 - 3
- >3

Peat Depth (m)

- 0
- 0 - 0.5
- 0.5 - 1
- 1 - 1.5
- 1.5 - 2
- 2 - 2.5
- 2.5 - 3
- > 3



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MUINGMORE WIND FARM

PEAT MANAGEMENT PLAN

PEAT DEPTH DETAILED

FIGURE 6-3-3i

Scale 1:2,500 @ A3

Date MARCH 2026

0 100 200

Meters

402.064443.00001.0128.0 Peat Depth Detailed

476800 477000 477200 477400

822200

822000

821800

20

T12

N

LEGEND

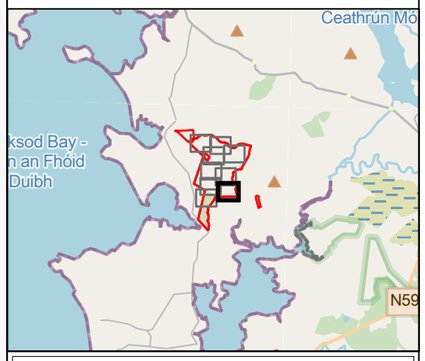
Proposed Development Site Boundary
Proposed Turbine Location
Proposed New Access Track
Proposed Crane Pad
Proposed Drainage Feature
Proposed Attenuation Basin

Peat Probe Depth (m)

0
0 - 0.5
1 - 1.5
1.5 - 2
2 - 2.5
2.5 - 3
>3

Peat Depth (m)

0
0 - 0.5
0.5 - 1
1 - 1.5
1.5 - 2
2 - 2.5
2.5 - 3
> 3



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MUINGMORE WIND FARM

PEAT MANAGEMENT PLAN

PEAT DEPTH DETAILED

FIGURE 6-3-3j

Scale 1:2,500 @ A3

Date MARCH 2026

0 100 200

Meters

402.064443.00001.0128.0 Peat Depth Detailled

Annex A Excavated Materials Calculations

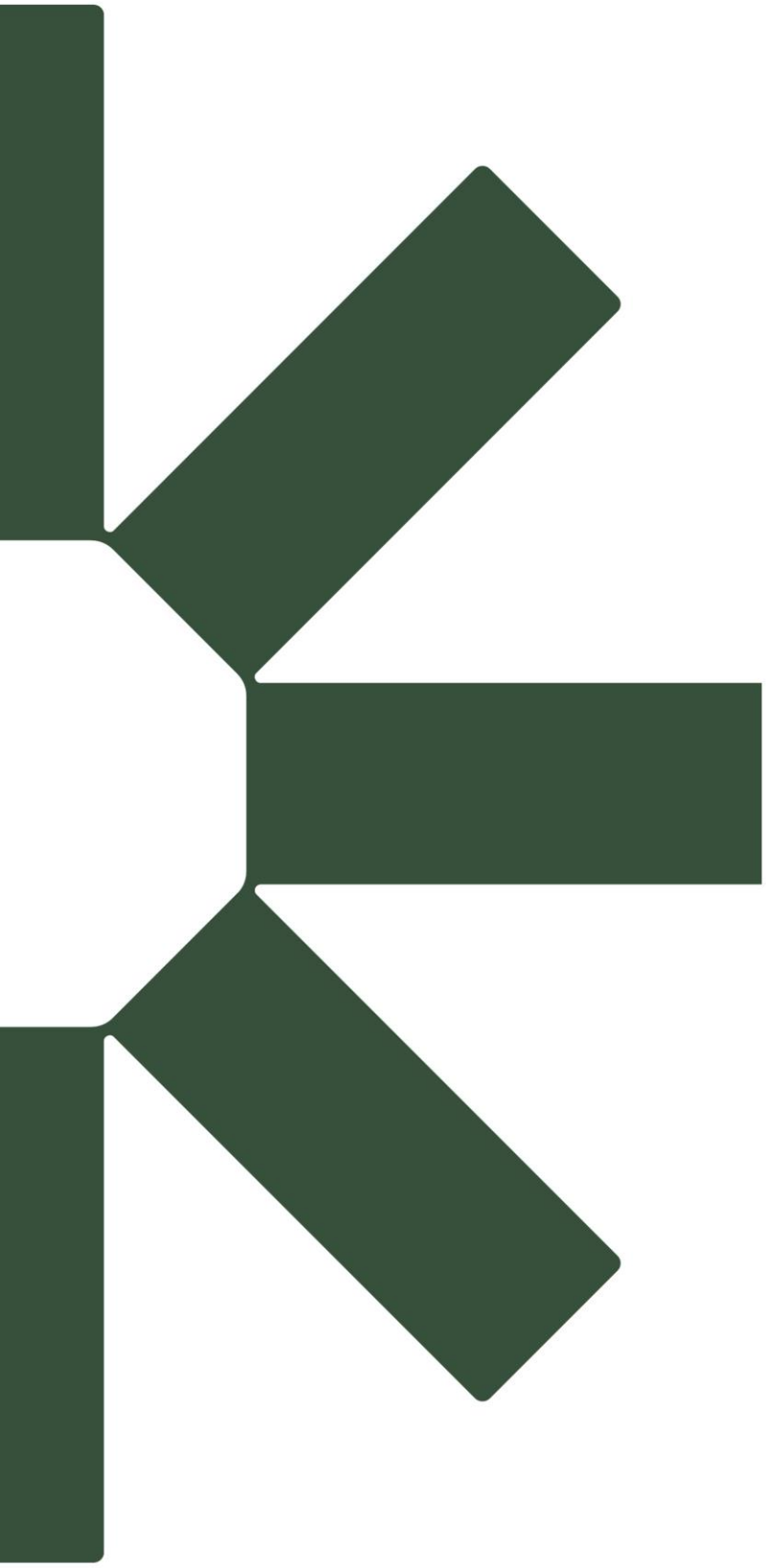
Technical Appendix 6.3: Peat Management Plan

Muingmore Wind Farm

RWE Renewables Ireland Limited

SLR Project No.: 501.065301.00001

Infrastructure on Peat	Length (m)	Width (m)	Area (m^2)	Average Depth of Peat (m)	Number	Total Excavated Volume Material (m^3)	Length (m)	Width (m)	Area (m^2)	Average Thickness of Peat (m)	Number	Total Re-use Volume of Material (m^3)	Notes
New Access Track (to be floated)	8758	6.5	56927	0.00	1	0	8758	1	8758	0.50	2	8758	Assumes all tracks on site where peat >1.0m and <5 deg slope will be floated construction.
Turbine Foundations			380	2.56	13	12644	1	70	70	0.50	13	455	To be excavated and peat placed 1m spread around the circumference of turbine.
Crane Hardstandings (to be floated)			3117	0.00	11	0						0	To have a floated foundation solution, no peat excavations required.
Blade Laydown Areas (to be floated)			4002	0.00	11	0						0	To have a floated foundation solution, no peat excavations required.
Blade Laydown Fingers (to be floated)			80	0.00	11	0						0	To have a floated foundation solution, no peat excavations required.
Crane Pad (to be floated)			492	0.00	11	0						0	Crane pad to be piled, removing requirement for peat excavations
Crane Hardstandings (to be cut)			3117	1.38	2	8603		2	400	1.38	2	2208	To be re-used in local area
Blade Laydown Areas (to be cut)			4002	1.38	2	11046			4002	1.38	2	11046	To be fully reinstated
Blade Laydown Fingers (to be cut)			80	1.38	2	221			80	1.38	2	221	To be fully reinstated
Crane Pad (to be cut)			492	1.38	2	1358		2	80	1.38	2	442	To be re-used in local area
Battery Energy Storage System (BESS)			13789	2.10	1	28957	380	1	380	1.00	1	380	To be re-used within local area. To be used within peatland restoration as detailed within Chapter 5: Biodiversity and Technical Appendix 5.5 Habitat and Species Management Plan.
Substation			11993	2.50	1	29983	370	1	370	1.00	1	370	To be re-used within local area. To be used within peatland restoration as detailed within Chapter 5: Biodiversity and Technical Appendix 5.5 Habitat and Species Management Plan.
Temporary Construction Compound (TCC) 1			9600	0.00	1	0						0	To have a floated foundation solution, no peat excavations required.
Temporary Construction Compound (TCC) 2			9600	0.00	1	0						0	To have a floated foundation solution, no peat excavations required.
Met Mast			73	0.00	1	0						0	To have a floated foundation solution, no peat excavations required.
Attenuation Ponds Turbines			1136	0.70	13	10338						0	To be used within peatland restoration as detailed within Chapter 5: Biodiversity and Technical A
Attenuation Pond BESS			1321	0.70	1	925						0	To be used within peatland restoration as detailed within Chapter 5: Biodiversity and Technical A
Attenuation Pond Construction Compounds			2025	0.70	2	2835						0	To be used within peatland restoration as detailed within Chapter 5: Biodiversity and Technical A
Attenuation Ponds IPP Compound			180	0.40	1	72						0	To be used within peatland restoration as detailed within Chapter 5: Biodiversity and Technical A
Attenuation Ponds Substation Compound			200	0.50	1	100						0	To be used within peatland restoration as detailed within Chapter 5: Biodiversity and Technical A
Peatland Restoration						0						101301	As detailed within Chapter 5: Biodiversity and Technical Appendix 5.5 Habitat and Species Management Plan.
Totals						**107080**						**125180**	



Making Sustainability Happen